

MEHMET SITKI MERDİVENCİ

6th EMship cohort: October 2015 – February 2017

Design and Optimization of Composite Base Frames & Shaft of Wind Turbine for Catamaran

Supervisor: Prof. Hervé Le Sourné, L'Institut Catholique d'Arts et Métiers, Nantes, France

Reviewer: Prof. Robert Bronsart, University of Rostock, Rostock, Germany

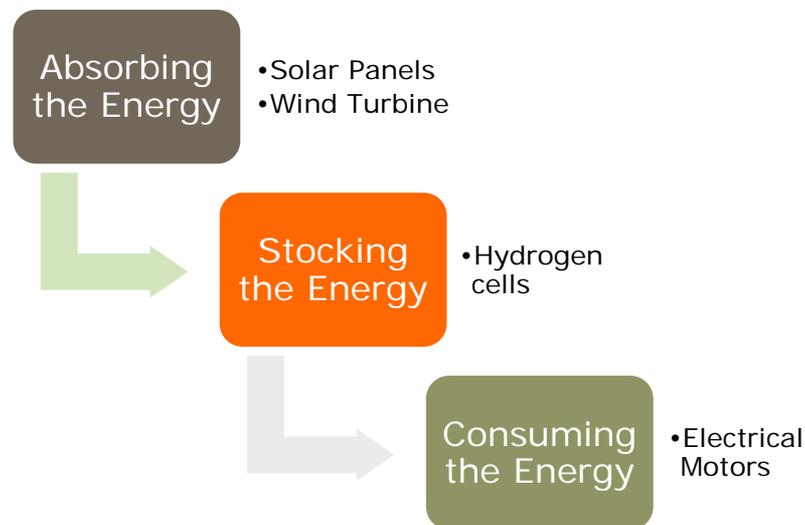
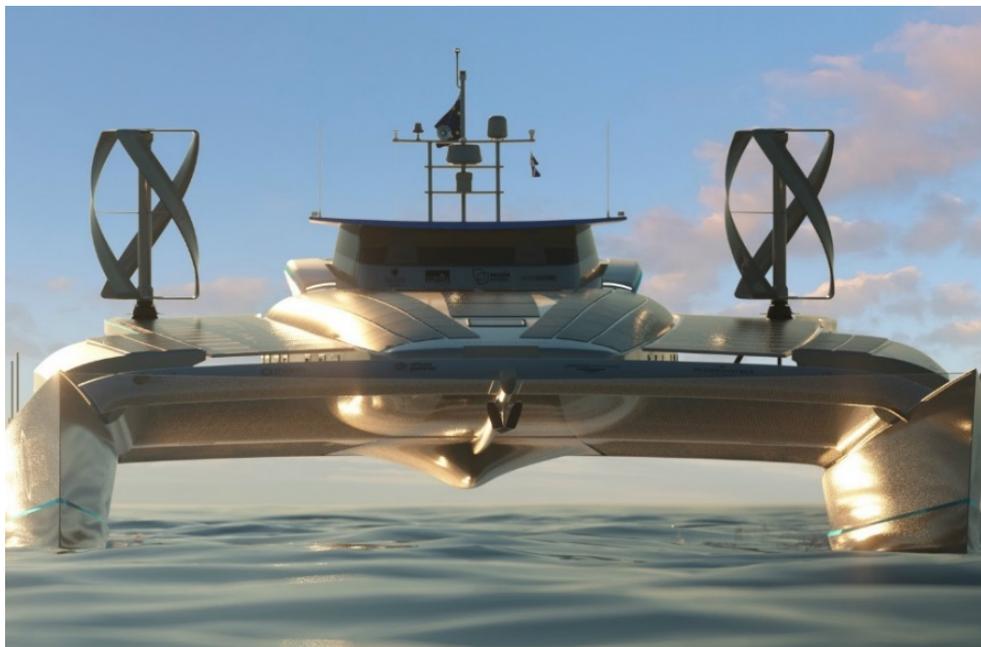
EMShip Meeting, Rostock, February 2017

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Introduction

Energy Observer



1. History of The Boat

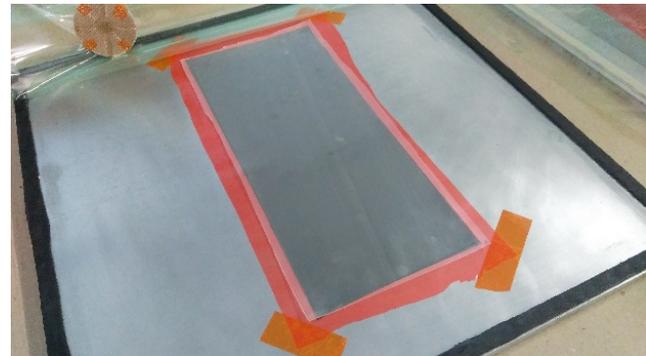
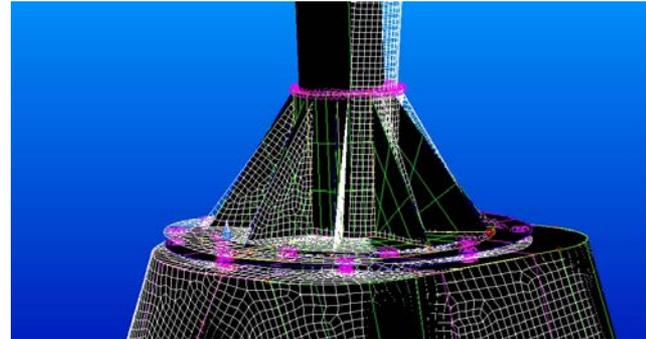
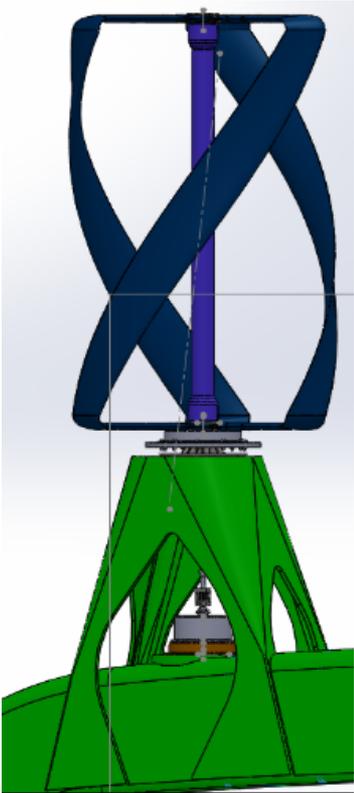
Formule Tag (1983)



- *24 m long*
- *Jules Verne Trophy 75 days (1994)*

2. Main objectives of the study

- Design & Structural Analyzes of Vertical Axis Wind Turbine and Its Support
- Investigation of damping material selection



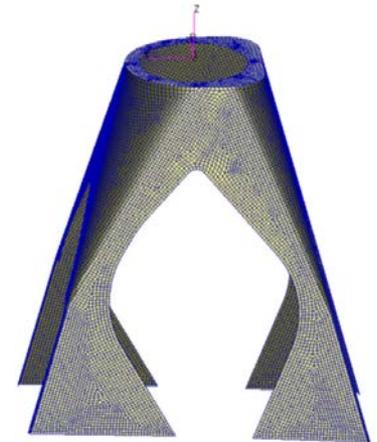
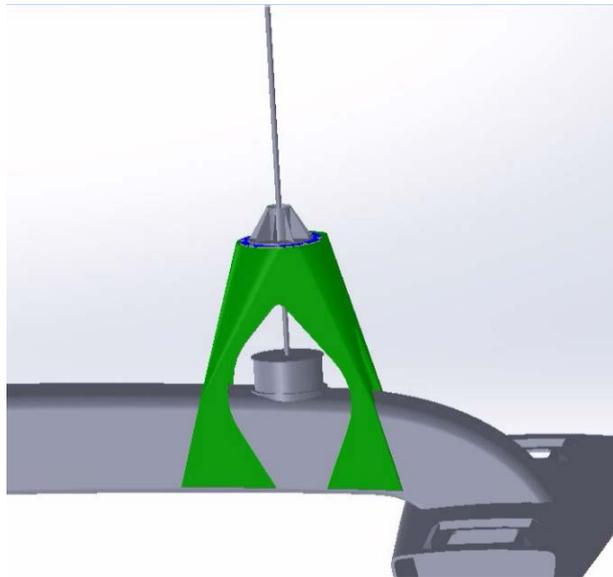
3. Presentation of Wind Turbine and Its Finite Element Model

Aerojoules

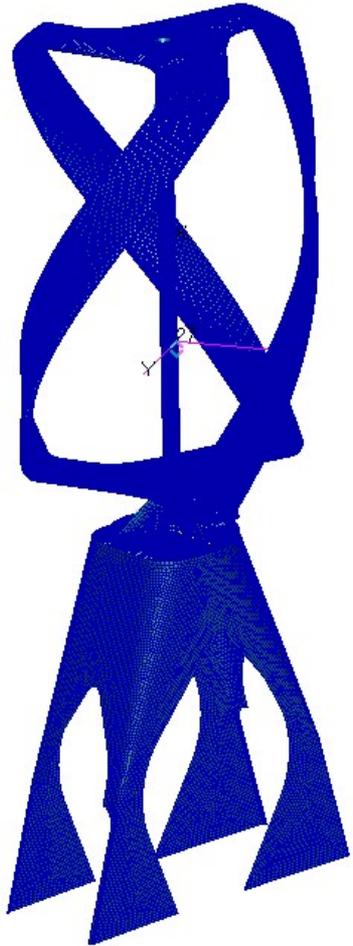


Adaptation of Aerojoules to Energy Observer

- Designing an Appropriate Support
- Using composite shaft



3. Presentation of Wind Turbine and Its Finite Element Model



Expected Minimum Bending Natural Frequency

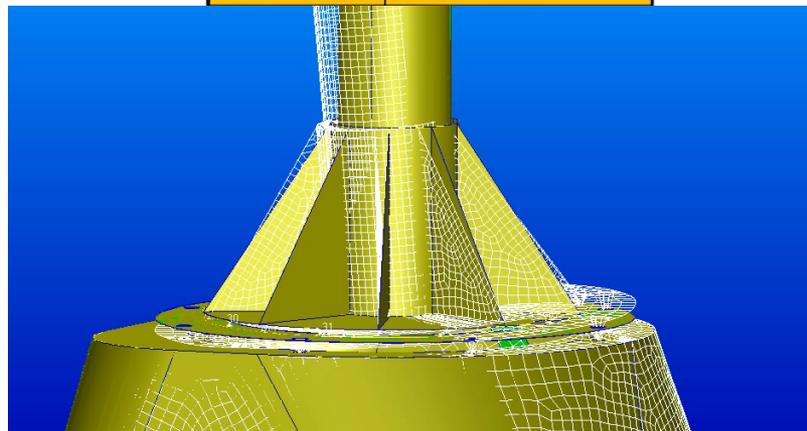
Maximum Rotation of Turbine : 300 RPM

Frequency = $n(\text{blades}) \times \text{RPM} / 60$

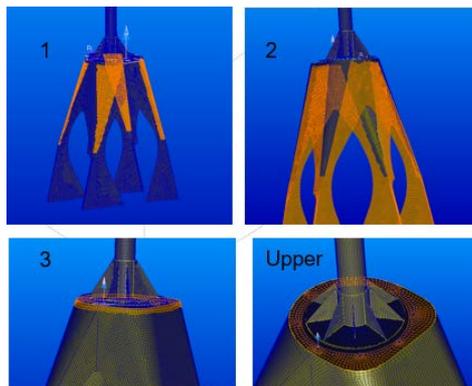
$3 \times 300 \text{ RPM} / 60 = 5 \text{ RPS}$

$5 \times 3 = 15 \text{ Hz}$

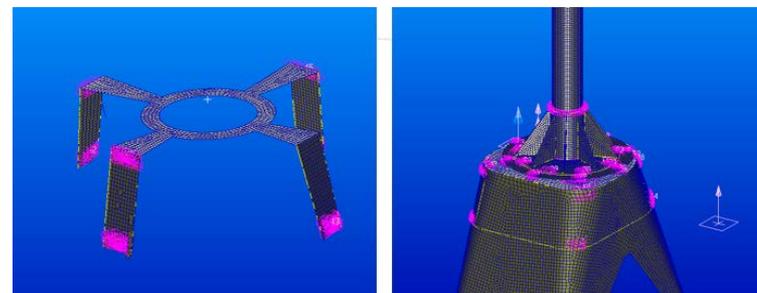
Modes	Frequency (Hz)
Mode 1	9.3
Mode 2	9.6



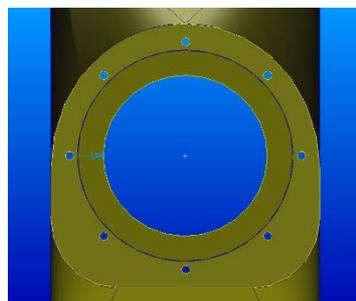
3. Presentation of Wind Turbine and Its Finite Element Model (Modifications)



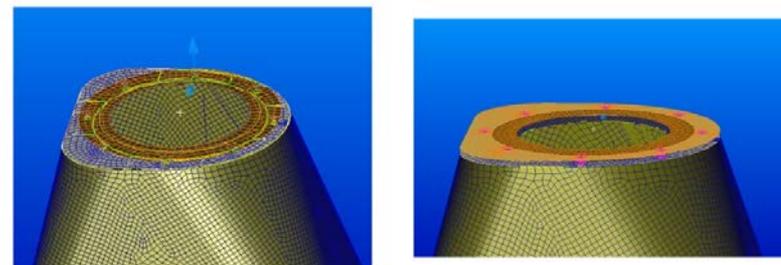
1st Bending Mode : 11,6 Hz
2nd Bending Mode : 11,7 Hz



1st Bending Mode : 11,9 Hz
2nd Bending Mode : 12,2 Hz



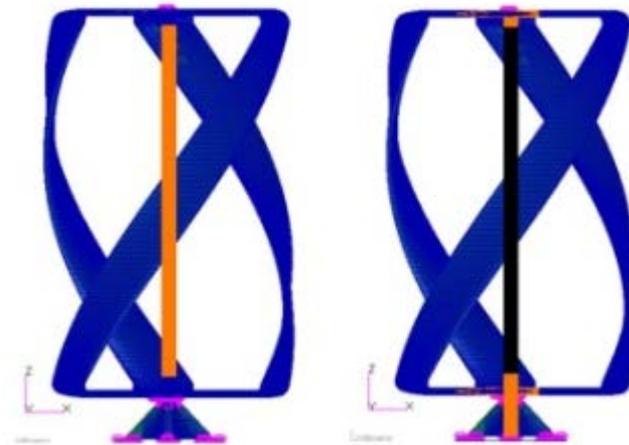
1st Bending Mode : 10,9 Hz
2nd Bending Mode : 11,3 Hz



1st Bending Mode : 12,1 Hz
2nd Bending Mode : 12,4 Hz

4. Parametric Study of Composite Fixed Shaft

- Carbon epoxy composite material
- 80 mm of external diameter
- Same behavior as Aerojoules



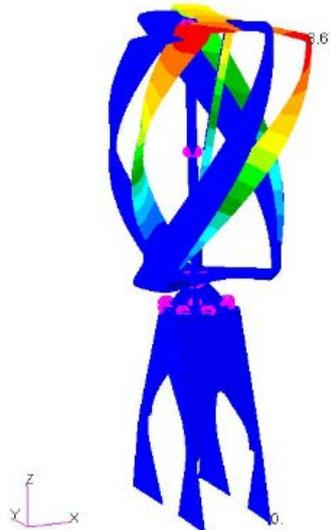
Thickness (mm)	1 st Mode Frequency (Hz)	2 nd Mode Frequency (Hz)	3 rd Mode Frequency(Hz)	Stacking Sequence
16	9 (180 rpm)	9,2 (184 rpm)	16 (320 rpm)	$([-30,0,30,0]_4, [45,0-45,0])_5$
16	9,1 (182 rpm)	9,3 (186 rpm)	16 (320 rpm)	$([-30,0,30,0])_5$
24	9,6 (192 rpm)	10 (200 rpm)	16,5 (330 rpm)	$([-30,0,30,0]_6, -30,0, [45,0-45,0])_5$
24	9,7 (194 rpm)	10 (200 rpm)	16,5 (330 rpm)	$([-30,0,30,0]_7, -30,0)_5$

5. Static and Dynamic Analysis of Entire Optimized Model

Bending Modes

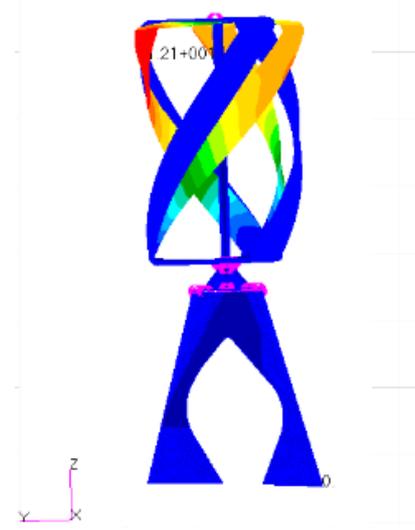


9.1 Hz
(182 RPM)
RPM)



9.3 Hz
(186 RPM)

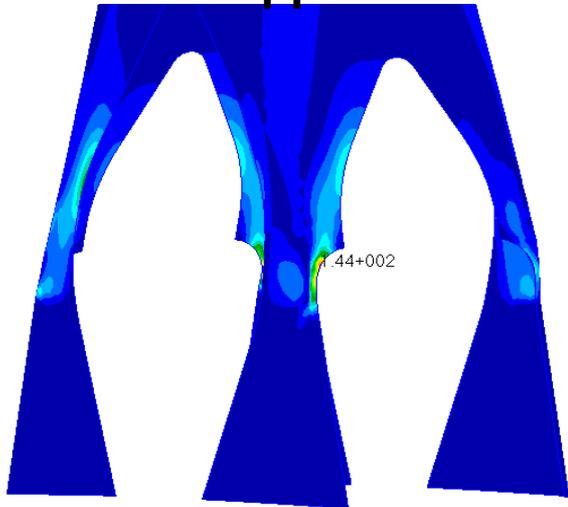
Flexion Modes



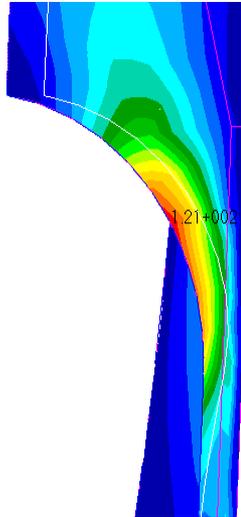
9 Hz
(180

5. Static and Dynamic Analysis of Entire Optimized Model

Stresses on Composite Support



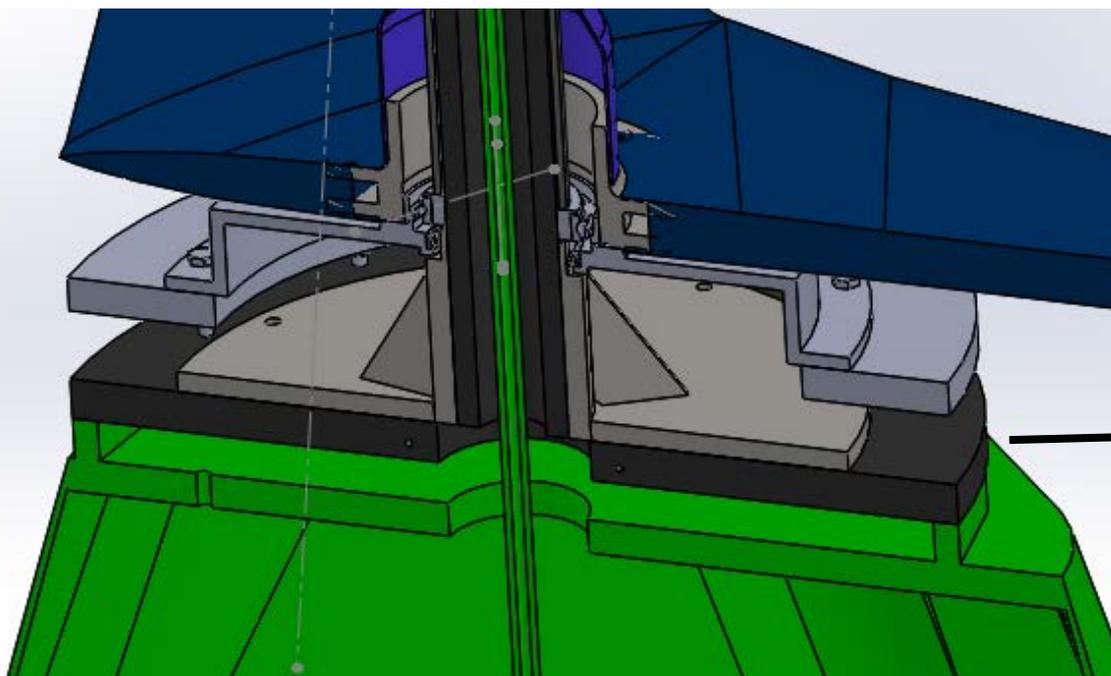
144 MPa
1st Layer



121 MPa
3rd layer

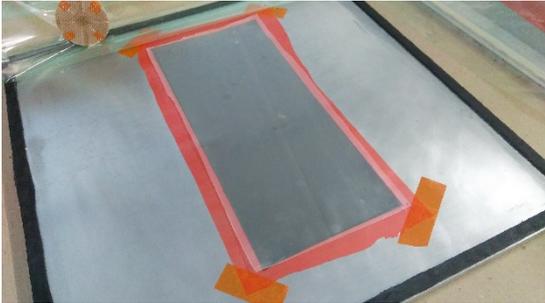
- Elastic limit of composite material: 603 MPa
- Less than 25 % of Elastic limit

6. Investigation of a Damping Material Selection



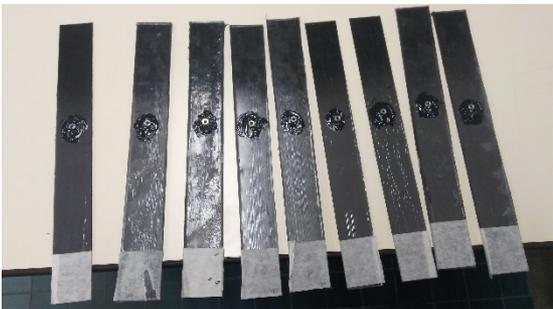
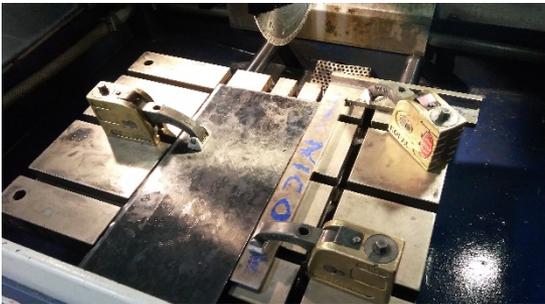
Carbon composite
with viscoelastic
material

6. Investigation of a Damping Material Selection



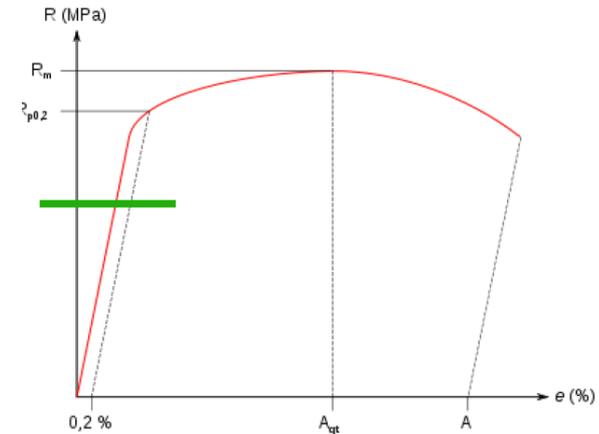
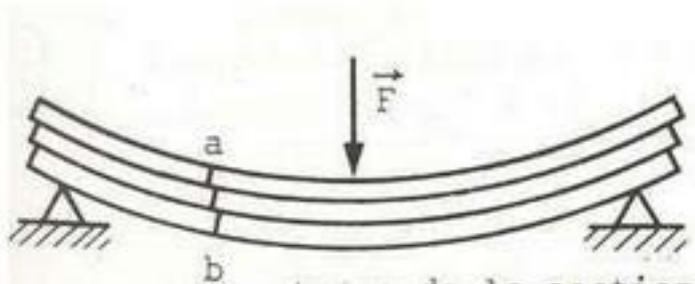
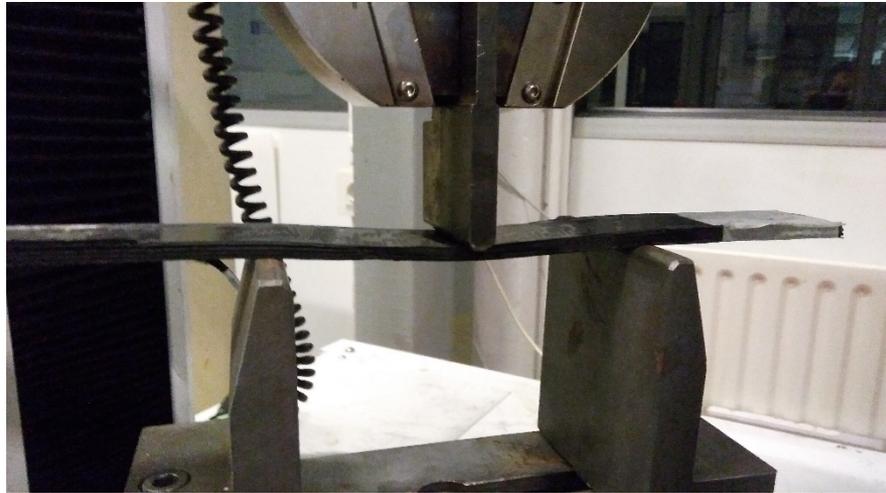
3 different type of samples:

- 0 layer of DYAD
- 2 layers of DYAD
- 4 layers of DYAD



6. Investigation of a Damping Material Selection

Flexion 3 points



$$E_{0D} = 72 \text{ GPa}$$

$$E_{2D} = 1,3 \text{ GPa}$$

$$E_{4D} = 0,33 \text{ GPa}$$

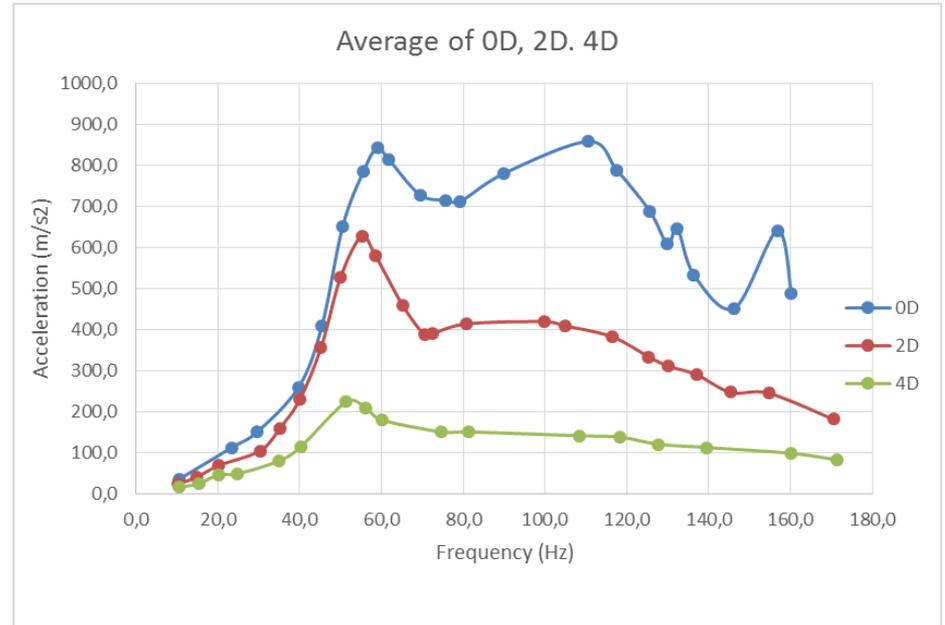
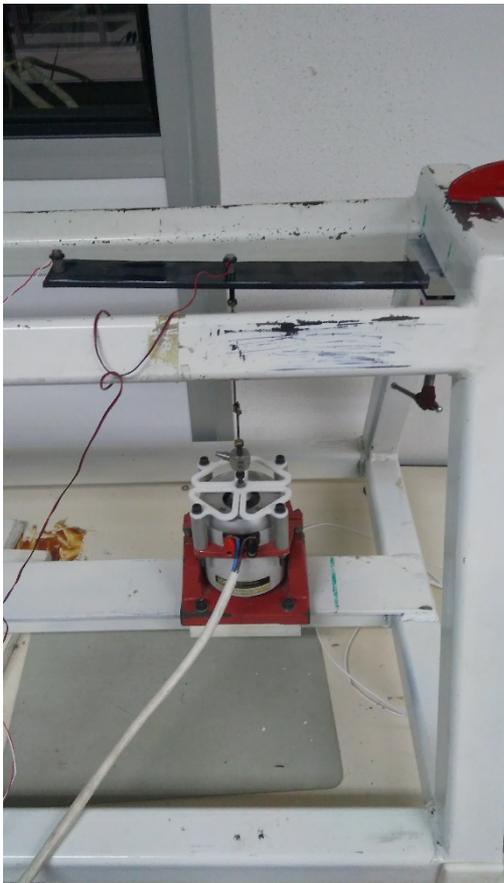
Shear Modulus of DYAD:

$$\tau = 0,33 \text{ Mpa}$$

(Steel = 70000 MPa)

6. Investigation of a Damping Material Selection

Frequency Response Analyses Experiment

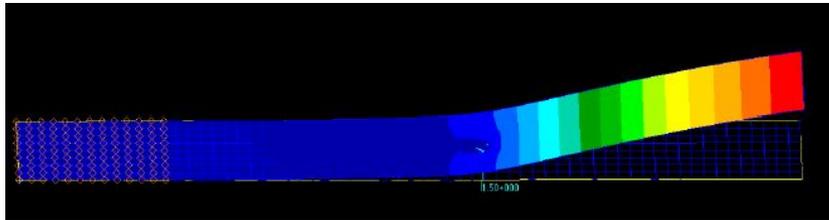


Samples	1st Natural Frequencies
0D	58.9 Hz
2D	55.1 Hz
4D	52 Hz

7. Comparison between Experimental and Numerical Results

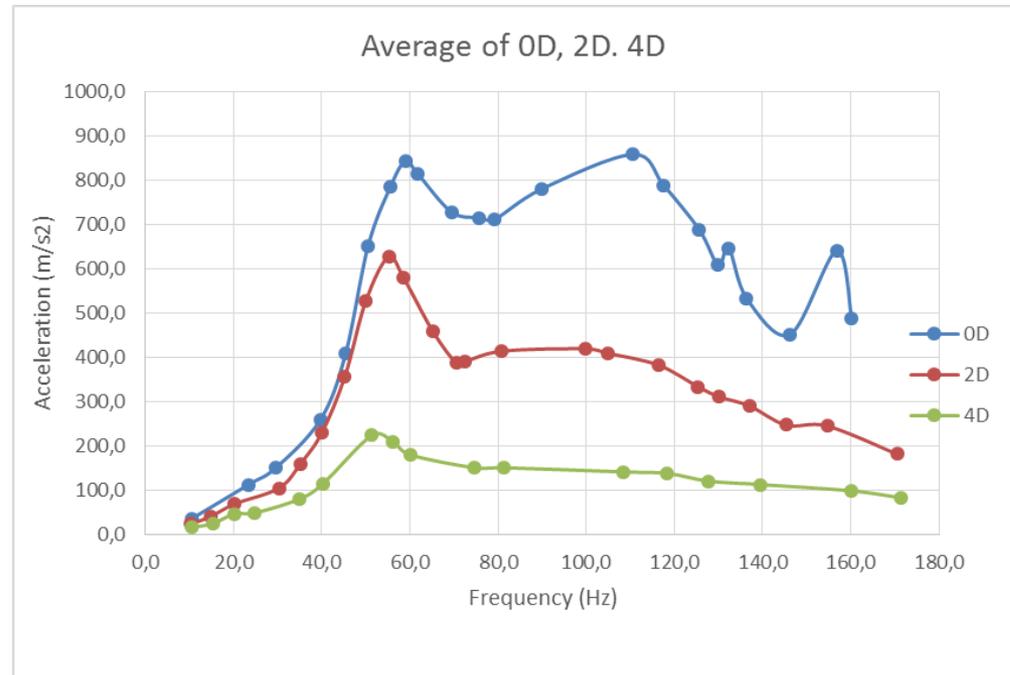
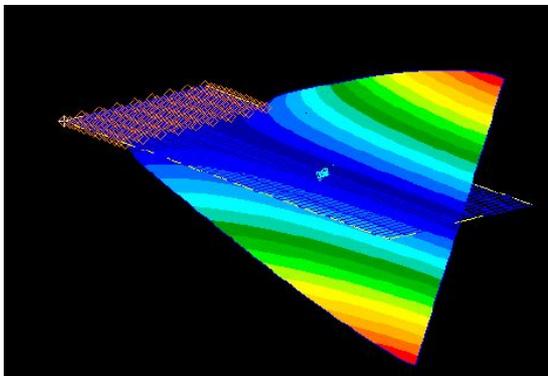
2D Sample

First Bending Mode at 53.5 Hz



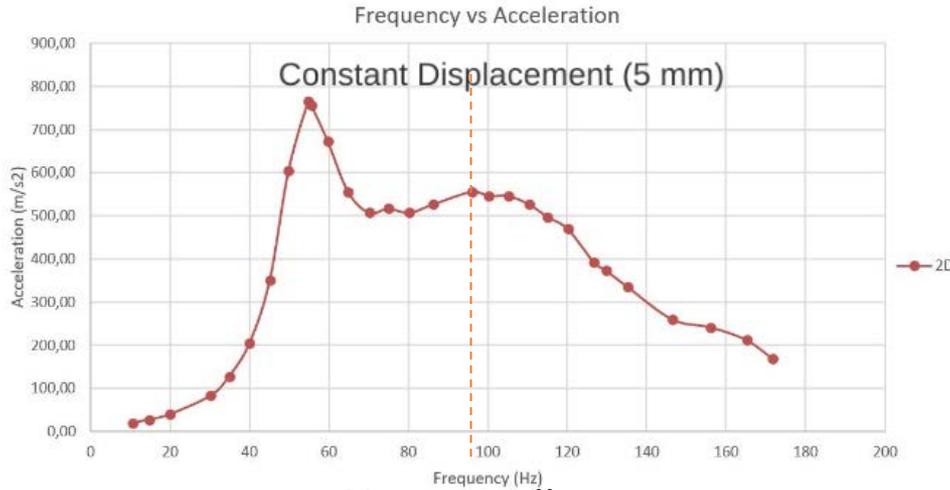
Samples	1st Natural Frequencies
0D	58.9 Hz
2D	55.1 Hz
4D	52 Hz

Torsion Mode at 86.3 Hz

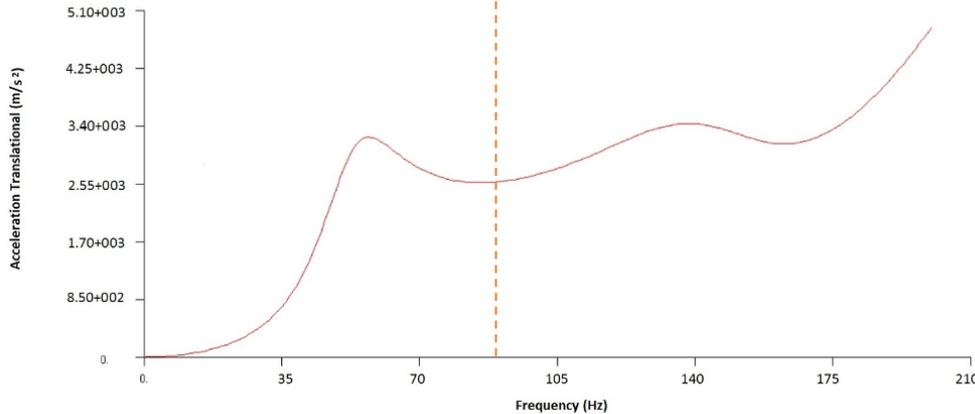


7. Comparison between Experimental and Numerical Results

Experimentally



Numerically

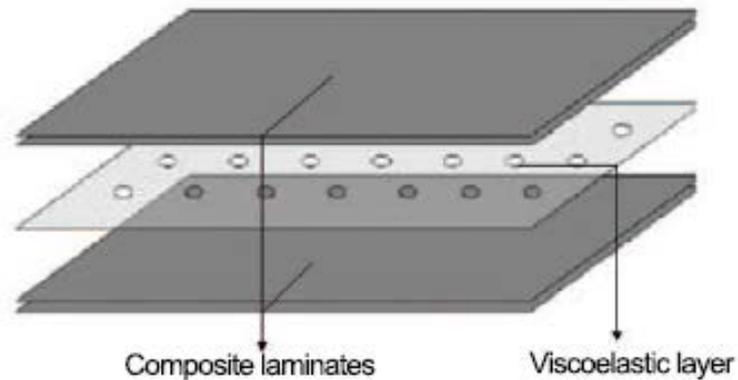
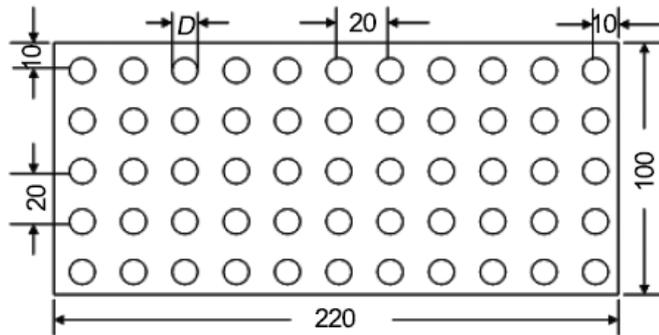


8. Conclusions

- Using more composite layers or having an interior structure of a composite support does not increase sufficiently the stiffness of entire system and consequently the first natural frequency.
- Implemented viscoelastic material increases the damping characteristics of carbon epoxy composites, however it causes a significant decrement on Young's modulus.

9. Future Work

Perforation of small holes on DYAD 601 (Pan & Zhang 2009)



Thank you.